PATENT SPECIFICATION

DRAWINGS ATTACHED

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COMPLETE SPECIFICATION

A Compression Ignition Engine Fuel System

We, Caterpillar Tractor Co., a corporation organized and existing under the laws of the State of California, United States of America, of 800 Davis Street, San 5 Leandro, State of California, United States of America, do hereby declare the invention, for which we pray that a patent may be granted to us, and the method by which it s to be performed, to be particularly

10 described in and by the following statement: This invention relates to engine fuel systems and particularly to a fuel system for a compression ignition engine which may be required to burn different kinds of fuel

Military specifications for engines often require that they be capable of operating on a wide variety of fuels for tactical purposes and in emergencies. Compression ignition type engines are best adapted to multi-fuel 20 operation but difficulties arise with fuels of

low cetane rating. The cetane number of a fuel is an indication of its ability to ignite under compression and gasoline with a very low cetane rating is extremely difficult to 25 ignite by compression. On the other hand, fuel oils and lubricating oils have high

cetane ratings. It is impractical and undesirable to build engines with sufficiently high compression ratio to insure ignition by 30 compression of gasoline under all operating

conditions. Since gasoline is frequently available in abundance as compared to other fuels, the desirability of including it as a fuel for military purpose is evident.

It has been recognized that the addition of even a small quantity of fuel of relatively high cetane number added to gasoline fuel greatly improves its performance in a compression ignition engine. However even

40 a small quantity of oil added continuously over long periods of operation requires that a large stock of oil be available.

Tests leading to the conception of the

present invention have shown that low cetane rated fuels result in satisfactory operation of low compression ratio engines 45 operation of low compression ratio engines under some operating conditions. For example a turbocharged engine of the precombustion chamber type with low compression ratio operates satisfactorily on low cetane fuel at low speeds, for example 50 1,000 rpm and lower. It also operates well at high speed except in the event of low manifold pressure, say five inches Hg

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It is therefore the object of the present 55 invention to provide an engine fuel system with improved means for injecting small quantities of a secondary fuel with the regular fuel and to provide means for introducing the secondary fuel only under certain 60

operating conditions.

It is a further object of the invention to provide means for introducing a small quantity of secondary fuel into the primary fuel supply at a point proximate to the 65 injection of fuel into the engine combustion

Further objects and advantages of the invention and the manner in which it is carried into practice are set forth in the 70 following specification wherein the invention is described in further detail by reference to the accompanying drawing.

In the drawing:
Fig. 1 is a schematic plan view of a 75 compression ignition engine and fuel system therefor embodying the present invention; Fig. 2 is a schematic view illustrating a

portion of a fuel pump and showing an injection nozzle and mechanism of the 80 present invention associated with the pump and nozzle for introducing small quantities of a secondary fuel into the regular fuel of

Referring first to Fig. 1 of the drawing, 85

under control of the spool valve 40. Com-

in the mixing valve and the manifolds 36 and 43 is normally closed by check balls 45 because the pressure in the line 18 is

normally greater than the pressure delivered

60 munication between the valve chamber 34

1,150,043 to the manifold by either of the pumps 15 65 an engine is generally indicated at 10 as ог 39. having an intake manifold 11 and an exhaust manifold 12. The engine also has In order to introduce a small quantity of secondary oil from the manifold 36 into the 5 A combined fuel pump and governor housing is shown at 14 and a fuel transfer pump 15 delivers fuel from a tank such as passage leading to the injection nozzle 30; a momentary condition of low pressure is 70 created in the line 18 once for each stroke of the plunger 26. This is accomplished by indicated at 16 to the fuel pump housing wherein individual fuel pumps direct the 10 fuel under pressure through lines 18 to the several combustion chambers of the engine. providing what is known as a skirt on the check valve 27. This skirt is in the form of a solid cylindrical portion 47, adjacent 75 The quantity of fuel injected upon each stroke is controlled by a governor (not shown) in the housing 14, the setting of which may be changed as by a foot pedal 20 and connecting linkage shown at 21. the conventional tapered valve seat, which slidably fits the bore in which the valve is disposed. As a consequence, the valve opens under pump pressure only after the skirt leaves the bore and, upon return of the 80 valve under influence of spring 28, closing The injection system is shown in greater detail in Fig. 2 wherein the pump housing takes place when the skirt enters the bore. Further movement of the valve until its 14 is shown as having a manifold 23 to tapered portion seats slightly increases the space volumetric capacity of the enclosure 85 20 which fuel is delivered by the transfer pump 15. A passage 24 communicates between which includes the line 18 and all of the the manifold and the pump cylinder 25 in space between the valve and the injection which a plunger 26 is reciprocated by cam nozzle 30. The orifice of the injection nozzle action in a well known manner. As the is also closed by a spring closed check valve 25 plunger is reciprocated, fuel is compressed 46 in accordance with conventional practice, 90 in the cylinder and injected through a check valve 27 normally closed by a spring 28. This pressurizes the fuel in the line 18 Thus a momentary pressure drop takes place in this otherwise highly pressurized space and one or the other of the balls 45 which leads to an injection nozzle 30. The 30 injection nozzle is disposed within the will, upon leaving its seat, permit inflow of fuel from either the manifold 36 or the 95 manifold 43. This type of skirted check valve has previously been used to cause a slight pressure drop after each injection combustion space of the engine where the fuel is ignited by compression. The present invention provides a mixing valve, generally indicated at 32, for introstroke of the plunger to prevent dribbling of 35 ducing small quantities of a secondary fuel with high cetane rating when it is required by engine operating conditions. This fuel caused by residual pressure behind the 100 valve in the nozzle. However in the present case the skirt on the valve is slightly longer mixing valve comprises a cross shaped body than that previously used and produces sufficient cavitation to induce flow through having a passage 33 connecting the line 18
40 with the injection nozzle 30 and intercepting
a valve chamber 34. The valve chamber the mixing valve. As illustrated in Fig. 2, the manifold 36 communicates with a passage 35 and manifold 36 (see also Fig. 1) which comwhich supplies the secondary fuel of high tetane rating is shown as closed by the spool valve 40 and a solenoid 50 is shown municates between mixing valves 32
45 associated with each of the injection nozzles for actuating this valve. As shown in Fig. 110 and with a source of supply of a suitable secondary fuel which may be lubricating oil 1, the solenoid actuated valve 40 is included in the circuit which includes a battery 51 and two switches 52 and 53 in series. The in the engine sump represented at 38 in Fig. 1. Fuel from this supply is delivered to the switch 52 is disposed for actuation by the 50 mixing valves by a pump 39 and under control of a valve 40 which may be, as governor control pedal 20 at a point where 115 the pedal has been depressed to cause engine illustrated in Fig. 2, a spool-type valve. The operation at a speed of say 1,000 rpm at which ignition failure might be expected mixing chamber also has a passage 42 for communication between the chamber 34 and with the low cetane fuel. However, since 55 a manifold 43 which communicates with all ignition failure is not expected except in 120 of the mixing valves and the fuel tank 16 the event of low intake manifold pressure, so that the manifold is pressurized by fuel transfer pump 15. This line 43 is also

the switch 53 is pressure actuated to an open position and closes only upon reduction

of pressure in the intake manifold to a point

conditions prevailing which tend to provoke

usually accompanied by ignition failure, 125 such for example as 5" Hg gauge. Thus with both the speed and low pressure

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ignition failure, both switches are closed and the solenoid 50 is actuated to communicate pressure to the manifold 36 and thus permit introduction to the fuel system of a small quantity of high cetane fuel for each stroke of the arms allures.

of the pump plunger.

During normal operation when ignition failure is not expected, the manifold 43 is pressurized because of the normal position

pressurized because of the normal position 10 of the valve 40 shown in Fig. 2 and the momentary low pressure condition between the fuel pump and the injection nozzle simply causes the introduction of a small quantity of the low cetane fuel upon which

15 the engine is operating.

It is possible to eliminate that portion 42 of the mixing valve which introduces the low cetane fuel; however the construction shown is preferred because it insures that

20 the volume and pressure of fluid between the check valve 27 and the valve in the nozzle 30 is the same for each injection stroke of the plunger. This insures uniform timing and smoother engine operation.

The configuration of the mixing valve is exaggerated in the drawing because the actual clearances are quite small. In practice the balls do not leave their seats more than about .03 inch. The position of

30 the parts as shown in Fig. 2 is with the pump plunger approaching bottom dead center. Valve 27 has closed causing unseating of ball 45 to admit low cetane faul. The ball is reseated as the plunger 35 commences its upward or pressure stroke.

WHAT WE CLAIM IS:—

1. A fuel system in a multi-cylinder

 A fuel system in a multi-cylinder compression ignition engine having pump

means for a primary fuel, a conduit from the pump means to each cylinder, a source 40 of secondary fuel under pressure lower than the pressure delivered by said pump means, passage means communicating secondary fuel from the source to each of said conduits,

and check valve means in each said 45 passage means to admit secondary fuel to the conduits only at spaced intervals of low pressure of primary fuel in the conduits.

2. The combination of claim 1 with a source of primary fuel under pressure lower 50 than that delivered by the pump, passage means communicating such low pressure primary fuel from its source to each of said conduits, and check valve means in each said last named passage means to admit 55

said last named passage means to admit 55 low pressure primary fuel to the conduits only at spaced intervals of low pressure of primary fuel from the pump means.

3. The combination of claim 2 with 60 valve means controlling flow selectively of the low pressure primary and secondary fuels.

- 4. The combination of claim 3 in which the two check valves for low pressure fuels 65 for each conduit comprise two ball checks in opposite sides of a single chamber which intersects the path of flow of fuel from said conduits.
- 5. A fuel system in a multi-cylinder 70 compression ignition engine substantially as hereinbefore described having reference to the accompanying drawings.

MARKS & CLERK.

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